

Safe Load Table

8" x 16" flexicore SECTION

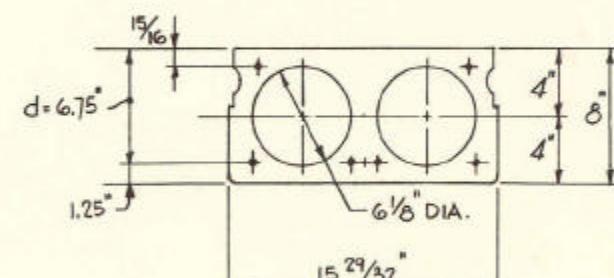
UNIFORMLY DISTRIBUTED SUPERIMPOSED* LOAD IN LBS. PER SQ. FT.

| STD. DESIGN- NATION | TENSILE STEEL AREA SQ. IN. | SIMPLE SPANS IN FEET AND INCHES | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---------------------------|----------------------------------|---------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | 10'-0" | 10'-6" | 11'-0" | 11'-6" | 12'-0" | 12'-6" | 13'-0" | 13'-6" | 14'-0" | 14'-6" | 15'-0" | 15'-6" | 16'-0" | 16'-6" | 17'-0" | 17'-6" | 18'-0" | 18'-6" | 19'-0" | 19'-6" | 20'-0" | 20'-6" | 21'-0" | 21'-6" | 22'-0" | 22'-6" | 23'-0" | 23'-6" | 24'-0" | 24'-6" | 25'-0" | 25'-6" |
| W 148 | 1.485 | | | | | 475 | 436 | 401 | 370 | 343 | 318 | 294 | 270 | 247 | 225 | 205 | 187 | 168 | 152 | 138 | 125 | 113 | 102 | 92 | 82 | 72 | 62 | 53 | 49 | 46 | 43 | 40 | |
| W 123 | 1.227 | | 558 | 506 | 460 | 420 | 384 | 353 | 324 | 298 | 274 | 254 | 235 | 217 | 202 | 187 | 174 | 161 | 150 | 140 | 128 | 116 | 104 | 93 | 83 | 73 | 64 | 55 | 49 | 46 | 43 | 40 | |
| W 99 | 0.994 | 550 | 494 | 445 | 403 | 365 | 332 | 303 | 277 | 253 | 233 | 213 | 196 | 181 | 167 | 154 | 142 | 131 | 121 | 112 | 104 | 96 | 88 | 81 | 75 | 69 | 63 | 54 | 48 | 45 | 42 | 40 | |
| W 92 | 0.920 | 508 | 455 | 410 | 370 | 335 | 305 | 278 | 253 | 232 | 213 | 194 | 179 | 164 | 151 | 139 | 128 | 118 | 109 | 100 | 92 | 85 | 78 | 72 | 66 | 60 | 55 | 50 | 46 | 42 | 38 | | |
| W 88** | 0.884 | 486 | 435 | 392 | 354 | 320 | 291 | 264 | 241 | 220 | 202 | 185 | 170 | 156 | 143 | 132 | 121 | 111 | 102 | 94 | 87 | 79 | 73 | 67 | 61 | 56 | 51 | 46 | 42 | 38 | | | |
| W 86 | 0.862 | 472 | 423 | 381 | 344 | 310 | 281 | 256 | 234 | 213 | 194 | 178 | 164 | 150 | 138 | 127 | 117 | 107 | 98 | 90 | 83 | 76 | 70 | 64 | 58 | 53 | 48 | 44 | 40 | 35 | | | |
| W 80 | 0.804 | 438 | 391 | 351 | 318 | 287 | 260 | 236 | 215 | 196 | 179 | 164 | 150 | 137 | 126 | 115 | 105 | 96 | 88 | 81 | 74 | 67 | 61 | 56 | 51 | 46 | 41 | 37 | | | | | |
| W 75 | 0.746 | 406 | 363 | 326 | 294 | 265 | 240 | 217 | 198 | 180 | 164 | 149 | 136 | 124 | 114 | 104 | 95 | 86 | 79 | 72 | 66 | 60 | 54 | 49 | 44 | 39 | 35 | | | | | | |
| W 74** | 0.742 | 403 | 359 | 323 | 291 | 262 | 237 | 215 | 196 | 178 | 162 | 148 | 135 | 123 | 113 | 103 | 94 | 85 | 78 | 71 | 65 | 59 | 53 | 48 | 43 | 39 | | | | | | | |
| W 69 | 0.693 | 373 | 334 | 298 | 269 | 242 | 219 | 198 | 180 | 163 | 148 | 135 | 123 | 111 | 101 | 92 | 84 | 76 | 69 | 63 | 57 | 51 | 46 | 41 | 36 | | | | | | | | |
| W 64 | 0.641 | 340 | 303 | 271 | 244 | 219 | 198 | 178 | 161 | 146 | 132 | 120 | 109 | 98 | 89 | 81 | 73 | 66 | 59 | 54 | 48 | 43 | 38 | 32 | | | | | | | | | |
| W 61** | 0.614 | 325 | 289 | 259 | 232 | 208 | 188 | 169 | 153 | 138 | 125 | 113 | 103 | 93 | 84 | 76 | 68 | 61 | 55 | 49 | 44 | 39 | 35 | | | | | | | | | | |
| W 59 | 0.589 | 310 | 276 | 247 | 221 | 198 | 178 | 160 | 145 | 131 | 118 | 106 | 96 | 87 | 78 | 71 | 63 | 57 | 51 | 45 | 40 | 35 | | | | | | | | | | | |
| W 54 | 0.543 | 282 | 251 | 223 | 200 | 178 | 160 | 144 | 130 | 116 | 105 | 94 | 85 | 76 | 68 | 61 | 54 | 48 | 43 | 37 | | | | | | | | | | | | | |
| W 50** | 0.497 | 255 | 226 | 201 | 180 | 160 | 143 | 128 | 115 | 103 | 92 | 82 | 73 | 65 | 58 | 51 | 45 | 40 | 35 | | | | | | | | | | | | | | |
| W 45 | 0.451 | 226 | 200 | 177 | 158 | 140 | 125 | 111 | 99 | 88 | 78 | 69 | 61 | 54 | 48 | 42 | 36 | | | | | | | | | | | | | | | | |
| W 41 | 0.411 | 202 | 179 | 157 | 139 | 123 | 109 | 97 | 86 | 75 | 67 | 59 | 52 | 45 | 39 | 33 | | | | | | | | | | | | | | | | | |
| W 39** | 0.393 | 190 | 167 | 147 | 130 | 114 | 101 | 89 | 79 | 69 | 61 | 53 | 47 | 40 | 34 | | | | | | | | | | | | | | | | | | |
| W 37 | 0.371 | 177 | 156 | 136 | 120 | 106 | 93 | 82 | 72 | 63 | 55 | 47 | 41 | 35 | | | | | | | | | | | | | | | | | | | |
| W 33 | 0.332 | 153 | 134 | 117 | 102 | 89 | 78 | 68 | 59 | 51 | 44 | 37 | | | | | | | | | | | | | | | | | | | | | |
| W 30** | 0.301 | 135 | 117 | 102 | 88 | 77 | 66 | 57 | 49 | 41 | 34 | | | | | | | | | | | | | | | | | | | | | | |
| W 22** | 0.221 | 84 | 71 | 60 | 50 | 41 | 33 | | | | | | | | | | | | | | | | | | | | | | | | | | |

*INCLUDES THE LIVE LOAD PLUS ANY DEAD LOAD THAT IS ADDITIONAL TO THE WEIGHT OF THE BARE GROUTED SLABS IN PLACE.

REMARKS

- Safe loads for greater steel content must not be extrapolated. A balanced slab has 1.705 sq. in. of steel for ACI Code allowables of 20,000 - 1688 - 8.
- Safe superimposed $w_g = \frac{5M}{L^3}$ = 56.3 lbs. (w_g in lbs. per sq. ft., M is in ft-lbs. per slab, L is in ft.)
- The maximum span without stirrups = $\frac{3320}{w_g + w}$. With stirrups used it is $\frac{8820}{w_g + w}$.
- The table is based upon dead load and grout of 75 lbs. per lin. ft. or $w_0 = 56.3$ lbs. per sq. ft.
- Stirrups are needed for all loadings above the heavy dashed line.
- The above tabulated load contemplate a depth, d, to the centroid of the steel of 6.75 in.
- Minimum total wall thickness (sl) = 3.22 in.
- Load computations are in accordance with 1951 ACI 318 CODE.
- Deflections in reinforced-concrete members under service loads depend on the elastic properties of concrete and steel, as well as on shrinkage and creep which, in turn, are influenced by temperature and humidity, curing conditions, age of concrete at the time of loading and other factors. Therefore, all simple methods of computation of deflection are necessarily approximate.
 - The safe loads above the solid stepped line have been reduced from the actual safe load as calculated in Item 2. This reduction improves the deflection characteristics under normal loading.
 - The elastic deflection (calculated on the basis of a cracked section) due to the design w_g only is not likely to exceed 1/360 of the span.
 - With an actual w_g of less than 40% of the design w_g and assuming an uncracked section, the total elastic deflection, due to the dead load of the slab and the actual w_g , is not likely to exceed 1/720 of the span.
 - Under the conditions described in (c) and using a long-time deflection multiplier of 2.0, the long time deflection is not likely to exceed 1/360 of the span.
- Indicates slabs with 2 rods tensile steel.



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